Lecture 30, Nov 24, 2022

Forced Convection

- Force convection is convection in which the fluid is imparted by external means, as opposed to natural convection which relies on natural fluid motion caused by density changes from temperature
- Up until now we've been using $Q = hA(T_i T_\infty)$ with h already given
 - -h could be measured experimentally in a complex system
 - Can we determine h based on system properties?
- Relevant properties:
 - Viscosity μ
 - Density ρ
 - Thermal conductivity k
 - Heat capacity c_p
 - Fluid velocity v_{∞} (for a free stream, outside the boundary layer)
 - Shape and size:
 - * Characteristic length (length of a plate, diameter of cylinder/sphere)
 - Type of flow (laminar vs turbulent)
- We need to consider the boundary layer, where the fluid slows down near the plate due to the no-slip condition at the boundary
 - We consider this as the region where $v < 0.99 v_{\infty}$
- At the interface between fluid and solid, heat transfer occurs only by conduction

$$\dot{q} = -k \frac{\partial I}{\partial u}$$

 $\partial y |_{y=0}$ - $\dot{q} = h(T_s - T_\infty)$ by Newton's law of cooling

- Therefore
$$h(T_s - T_\infty) = -k \frac{\partial T}{\partial y}\Big|_{y=0} \implies h = \frac{-k \frac{\partial T}{\partial y}\Big|_{y=0}}{\partial T}$$

- Now the problem becomes solving for $\frac{\partial I}{\partial y}$, but typically we don't know this

- Consider the boundary layer and assume $T_s > T_{\infty}$
 - We have both a velocity and a thermal boundary layer; we basically want the slope of this thermal boundary layer
 - Overall h changes with position as local $\frac{\partial T}{\partial y}$ at the surface changes, as the boundary layer develops (boundary layer gets thicker as the fluid flows further down the surface)
 - Define a local heat transfer coefficient x where x is along the surface, then the overall h is $1 f^L$ -|x|

$$h = \frac{1}{L} \int_0^{\infty} h(x) \, \mathrm{d}x$$

Boundary Layer Flow

- Typically the boundary layer begins with laminar flow, then becomes turbulent as you go down the surface, with a transitional region in the middle
- The fluid exerts a stress on the plate, $\tau = \mu \left. \frac{\partial v}{\partial y} \right|_{y=0}$
- We need to define a "friction coefficient" for the fluid By conservation of energy $\Delta(p\dot{v}) + \Delta\left(\frac{\dot{m}v^2}{2}\right) = 0$

$$-p - p_{\infty} + \frac{\rho v^2}{2} - \frac{\rho v^2_{\infty}}{2} = 0 \implies p - p_{\infty} = \frac{\rho v^2_{\infty}}{2}$$
* This $p - p_{\infty}$ is the force per unit area felt by the body
* $\frac{\rho v^2_{\infty}}{2}$ is the inertial force

 $-\frac{F}{4} = \tau = c_F \frac{\rho v_{\infty}^2}{2}$ where c_F is the friction coefficient for the fluid, defined for different shapes,

generally about 1

* For a sphere it's about 0.47, for a plate about 1.17, for a convex hull 2.3, for an airfoil 0.04

Diffusivities

- In molecular diffusion (mass transfer) we have Fick's law $J_A = -D_{AB} \frac{\mathrm{d}C_A}{\mathrm{d}x}$
 - D_{AB} is the mutual diffusion constant for A into solid B with units of m²/s
 - C_A is the concentration of A
- In heat transfer we have Fourier's law $\dot{q} = -k \frac{\mathrm{d}T}{\mathrm{d}x} \implies \dot{q} = \frac{k}{\rho c_p} \frac{\mathrm{d}}{\mathrm{d}x} (\rho c_p T) = -\alpha \frac{\mathrm{d}}{\mathrm{d}x} (\rho c_p T)$
 - α is the thermal diffusivity
 - $-\rho c_p T$ can be thought of as a "concentration of thermal energy", the amount of thermal energy per unit volume with units of J/m^3
- In a fluid μ is the dynamic viscosity; define $\frac{\mu}{\rho} = \nu$ to be the kinematic viscosity (aka momentum

diffusivity)

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- Shear stress is in general
$$\tau = \mu \frac{\mathrm{d}v}{\mathrm{d}y} = \frac{\mu}{\rho} \frac{\mathrm{d}}{\mathrm{d}y}(\rho v) = \nu \frac{\mathrm{d}}{\mathrm{d}y}(\rho v)$$

- This is the diffusion equation again
- $-\tau$ can be thought of as a "momentum flux"
- $-\rho v$ is the "concentration of momentum", momentum per unit volume