# Lecture 23, Nov 2, 2021

## **Curvature Diagrams**

- Like shear and moment diagrams, we can draw curvature diagrams
- Recall  $\phi = \frac{M}{EI}$ , so we can use this and the bending moment diagram to draw a curvature diagram (note EI is usually a constant, so the BMD and curvature diagrams are usually the same shape, just scaled by a constant; EI is not constant if the shape has a changing cross section or is not made of a uniform material)
  - The units of  $\phi$  is rad/mm
  - Curvature can have jumps due to changing EI, but the moment diagram is always continuous
- Note that the y in  $\sigma = \frac{My}{I}$  is not the same as the y in  $\phi = \frac{d^2y}{dx^2}$  (for small angles only); the first is internally in the member itself, the second is the deflection of the beam (y(x) is the displaced shape of the beam)

- If angles are not small, then 
$$\phi = \frac{\frac{\mathrm{d}^2 y}{\mathrm{d}x^2}}{\left(1 + \left(\frac{\mathrm{d}y}{\mathrm{d}x}\right)^2\right)^{\frac{3}{2}}}$$

- Angles are usually very small so  $\frac{dy}{dx}$  is small and even more so when squared; the difference it causes is usually less than the uncertainties of the material constants so it's irrelevant

- Even though we know the curvature, we still don't know the displaced shape y(x); to do this we need to double integrate, but this is a lot of work
  - Integrating  $\phi$  gets  $\theta$ , and integrating  $\theta$  gets us y(x)
  - Example: Consider a beam with a wkN/m distributed load on top; the max bending moment is  $\frac{wL^2}{2}$  can can be modelled by  $M(x) = \frac{x(L-x)w}{2}$

8 The curvature is 
$$\frac{x(L-x)w}{2EI} = \frac{wxL}{2EI} - \frac{wx^2}{2EI}$$
  
\*  $\theta = \int \phi \, \mathrm{d}x = \frac{wx^2L}{4EI} - \frac{wx^3}{6EI} + C_1$   
\*  $y = \int \theta \, \mathrm{d}x = \frac{wx^3L}{12EI} - \frac{wx^4}{24EI} + C_1x + C_2$ 

- \* Using our initial conditions,  $C_2 = 0$  and  $C_1 = -\frac{wL^3}{24EI}$
- \* To test this we can evaluate at  $x = \frac{L}{2}$ , since the structure is symmetric the slope should be 0 at this point

\* 
$$y(x) = \frac{wx^3L}{12EI} - \frac{wx^4}{24EI} - \frac{wL^3x}{24EI}$$
  
\* Note the signs might be weird

- Even though it might be easy in this case, it is usually very hard; in this case we had a single continuous equation for the bending moment, but if we had point loads or other more complex loading types there will be lots of pieces in the moment equation
- The moment equation is usually hard to obtain
- To get the shape more easily, we can use the two Moment Area Theorems

### First Moment Area Theorem $(\theta)$

- Since curvature  $\phi = \frac{d\theta}{dx}$  the change in slope over the change in length, so by the fundamental theorem of calculus, the change in slope between two points  $\Delta \theta_{AB}$  is the integral of the curvature
  - Note  $\theta(x)$  is the slope of the beam at x
- $\Delta \theta_{AB} = \int_{A}^{B} \phi(x) \, \mathrm{d}x$  is the first Moment Area Theorem, which states that the change in slope

between any two sections of a deflected beam is equal to the area under the curvature diagram between those two sections

- Note that since this method only gives us the change, we need a point where the slope is known
- Signs are not automatic and must be determined using intuition

## Second Moment Area Theorem ( $\Delta$ )

- Δ = ∫ θ dx so we can do an integration-like process
  θ is the area under the curve between two regions plus a constant C<sub>1</sub>
- $\Delta = \int (A + C_1) \, \mathrm{d}x$
- If we pretend that A is not a function of x, then we get  $Ax + C_1x + C_2$
- But since A is a function of x, we have to multiply by  $\bar{x}$  instead of x for  $A\bar{x} + C_1 x + C_2$ , where  $\bar{x}$  is the distance to the centroid of the area under the curvature diagram
- $C_1x + C_2$  is a line, which tells us that our answer is going to have a linear offset
- Geometrically this line is the tangent to the displaced shape at A
- Note  $\delta_{BA}$  has the displacement at B, the tangent at A, and the area under the curvature diagram between A and B
- If the area under the curve is complicated we can break it up into pieces and have  $\delta_{BA} = \sum_{i=1}^{n} A_i d_i$ ,

where  $A_i$  is the area of each piece and  $d_i$  is the horizontal distance between B and the centroid of the piece i

• For any two points A and B along the deflected beam, the tangential deivation of point B,  $\delta_{BA}$ , is equal to the product of the area under  $\phi(x)$  betweeen A and B, and the distance from the centroid of the diagram between A and B, to B (i.e. the first moment of area about point D)



Figure 1: Summary of Moment Area Theorem 2;  $\delta$  is the tangential deviation

# Areas and Centroids of Common Shapes

- When using these two theorems, the areas and centroids of many different shapes are needed; these are available in the appendix
- If the cross sections are more complex but can be broken down into a number of common shapes, then we can still apply the two Moment Area Theorems and sum up the contributions from each piece



Figure 2: Diagram of the derivation of the Second Moment Area Theorem

• 
$$\begin{cases} \Delta \theta_{AB} = \sum_{i=1}^{n} i = 1^{n} \left[ \int \phi(x) \, \mathrm{d}x \right]_{i} \\ \delta_{DT} = \sum_{i=1}^{n} \left[ \bar{x} \int \phi(x) \, \mathrm{d}x \right]_{i} \end{cases}$$