# Lecture 19, Oct 25, 2021

## **Damped Free Vibrations**

- Oscillating systems will eventually stop due to loss of energy by *damping*, which could be engineered or an inherent system property
- Damping is quantified by the damping ratio  $\beta$ , the ratio between the provided damping properties of the system and the minimum amount of damping to prevent it from oscillating completely
  - *Critical damping* is the amount of damping that can make the system stop oscillating the fastest
  - More damping (overdamped) will make the system reach equilibrium slower, and less damping (underdamped) will cause it to oscillate
- In civil structures  $\beta$  range from 0 to 0.05
- For a damped system, the differential equation becomes  $m \frac{d^2x}{dt^2} + 2\beta \sqrt{mk} \frac{dx}{dt} + kx = 0$  The solution is an exponentially decaying sinusoid with the form  $x(t) = Ae^{-\beta\omega_n t} \sin(\omega_d t + \phi) + \Delta_0$ ,
- where:
  - -A is the amplitude of oscillation
  - $-\beta$  is the damping ratio

$$-\omega_n$$
 is the natural frequency  $\sqrt{\frac{k}{m}}$ 

- $\phi$  is the phase delay
- $-\Delta_0$  is where the system naturally settles due to gravity
- $\omega_d$  is the *damped frequency*, related to  $\omega_n$  by  $\omega_d = \omega_n \sqrt{1 \beta^2}$ \* Since  $\beta$  is usually low in civil structures,  $\omega_d \approx \omega_n$

### **Forced Oscillations**

- In reality structures may be subjected to dynamic loading due to the movement of people etc; in the simplest case the load is sinusoidal with  $F(t) = F_0 \sin(\omega t)$
- Substituting the dynamic load into the equation:  $m\frac{\mathrm{d}^2x}{\mathrm{d}t^2} + 2\beta\sqrt{mk}\frac{\mathrm{d}x}{\mathrm{d}t} + kx = F_0\sin(\omega t)$
- The complete solution is outside the scope of this course but consists of the sum of two parts: the transient solution, which dominates when t is small, and the steady-state solution, which dominates when t is large and dictates the long-term behaviour of the system
- The steady state solution is more relevant to design and can be expressed as  $x(t) = \text{DAF} \cdot \frac{F_0}{k} \sin(\omega t + \omega t)$  $\phi$ ) +  $\Delta_0$ 
  - $\frac{1}{\sqrt{\left(1-\left(\frac{f}{f_n}\right)^2\right)^2+\left(\frac{2\beta f}{f_n}\right)^2}}, \text{ where } f \text{ is }$ - DAF is the *dynamic amplification factor*, calculated as

the driving frequency and  $f_n$  is the natural frequency of the system

- From the equation for the DAF we can see that the response of the system is strongly influenced

by  $\frac{f}{t}$ , as it influences both the frequency and the amplitude of the response through the DAF

## Resonance

- The DAF has the highest value when the driving frequency is approximately equal to the natural frequency, which leads to a very high increase in amplitude known as resonance
- Increasing the amount of damping increases  $\beta$  and reduces the DAF, especially the peak value at resonance
- The DAF is 1 when  $\frac{f}{f_n}$  is 0, and gradually becomes 0 as the ratio  $\frac{f}{f_n}$  becomes large, with a peak at  $\frac{f}{f_n} = 1$



Figure 1: Response to an input load with  $\frac{f}{f_n} = 2.5$  (left) and  $\frac{f}{f_n} = 0.5$ 



Figure 2: Influence of  $\frac{f}{f_n}$  on the DAF for various values of  $\beta$ 

# **Designing for Dynamic Effects**

- To check for dynamic effects, we don't need to solve the whole system; we just need to check whether the maximum stress results in failure
- Consider a set of dynamic loads  $w_{tot} = w_{sta} + w_0 \sin(\omega t)$ , where  $w_{sta}$  is the stationary component of loading, which does not vary in time, such as the dead load of the structure and the weight of a standing crowd of people;  $w_0$  and  $\omega_0$  is the dynamic load caused by, for example, a crow of people walking around
- When designing a pedestrian bridge the frequency of loading caused by walking is typically assumed to be 2Hz; therefore unless there is significant damping, having a natural frequency close to 2Hz can lead to large oscillations and possibly collapsing the structure
- The equivalent static load is then  $w_{eq} = w_{sta} + \text{DAF} \cdot \omega_0$  as the maximum amplitude of oscillation is scaled by the DAF
- The DAF can be calculated once the damping  $\beta$  and natural frequency  $f_n$  are determined; using the equivalent static load we can then check whether the members can withstand the stresses
- For a point load at the midspan, the natural frequency can be estimated to be  $f_n = \frac{15.76}{\sqrt{\Delta_0}}$ ; for a UDL

at the midspan  $f_n = \frac{17.76}{\sqrt{\Delta_0}}$ , where  $\Delta_0$  is the midspan deflection under  $w_{sta}$  in mm, i.e. how much the midspan of the structure deforms with just the static load